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Tormek grinder



More Math for the adjustable knife-jig

More Math for the adjustable knife-jig on the Tormek grinder

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I am very grateful to Ken Schroeder for the interest he has shown for my devel-opment and his contribution to improvements and alternatives. I would also like to thank the following members of the Tormek forum for their inspiring contribu-tions: "Wootz" (Vadim), "cbwx34" (Curtis) and "Jan" Acknowledgement

Document generated in free software office package: LibreOffice

In 2013 I bought a Tormek grinder and after some experimenting and grinding of the available knives, blades, scissors etc. it became clear to me that the reproducibility with the adjustable stop. If D is fixed, then the grinding angle can be adjusted by changing the distance K and D should be adjusted to So the grinding angle Δ is determined by: which can be simplified to: With the cosine-law we get radius R₁ is perpendicular to the tangent is equal to the angle between the knife blade and the tangent to the stone while the and via the long side D (= R_2 +S) back to the jig on the universal support. Consider the triangle determined by the knife jig, via R₁ to the centre of the stone be realized by measuring and adjusting the position of the universal support and the length of the adjustable jig. That resulted in the development of the following formuof the grinding angles was rather poor if the adjustment was done according to the ter "References" on page 15) That document will be further referred to as "Doc1". tings at different stone diameters and for a range of grinding angles. [1] (See chap-For easy application, the method was described in a document with tables for set The angle opposite side D (=S+R) is equal to $90^{\circ}+\Delta$ because the grinding angle Δ las That method however is not fast and easy. I wanted a simple method which could clears the bevel. bevel is coloured with a marker pen and the support is adjusted until the stone procedure described in the handbook. Good reproduction can be obtained if the adjustable Introduction stop grinding jig support universal Figure 1: Original diagram for jig adjustment adjustable ŝ ㅈ ⊳ clamp $D = \sqrt{(K^2 + R^2 + 2 * K * R * sin(\Delta))}$ $D^2 = K^2 + R_1^2 - 2 * K * R_1 * \cos(90^{\circ} + \Delta)$ $D^2 = K^2 + R^2 + 2 * K * R * sin(\Delta)$ -#SHR $\Delta = \arcsin\left|\frac{\mathsf{D}^2 - \mathsf{K}^2}{\mathsf{R}^2} - \mathsf{R}^2\right|$ R_2 00 tangent 꼬 2*X*R grinding stone ⊳ [F2] [F1] [F0] <u>ە</u> 6 [9] 2 About reference points References

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- [1] "Simple and accurate Grinding Angle Adjustment" Document "Doc1" on knife-jig adjustment, December 2013 https://bit.ly/2yX9dUC
- topic on Tormekforum, April 14, 2014 "Simple adjustment of the grinding angle" https://www.tormek.com/forum/index.php?topic=1849.0
- [3] "Thanks, Ton ("Dutchman")" topic on Tormekforum, September 12, 2014 https://www.tormek.com/forum/index.php?topic=2240
- [4] "Knife setting tool" topic on Tormekforum, May 25, 2015 https://www.tormek.com/forum/index.php?topic=2510
- [5] "Matching grinding wheels of different diameter" Introduction of Wootz method, March 28, 2016 https://www.tormek.com/forum/index.php?topic=2969
- https://www.tormek.com/forum/index.php?topic=3365.0 Introduction of Wootz applet "A new way to calculate knife jig set up"
- [7] "Wootz" website
- http://knifegrinders.com.au
- [8] "How to get razor-sharp knives on Tormek" by "Wootz" https://youtu.be/UckPmizIIk0 Movie-2 https://youtu.be/ZDPXqAK9Xr0 Movie-1 <u>https://www.tormek.com/forum/index.php?topic=3661.0</u> topic on Tormekforum
- Jan's Excel script

https://www.tormek.com/forum/index.php?topic=3365.msg20593#msg20593 Discussions about accuracy

[10] "Re: kenjig modification for paring knives"

https://www.tormek.com/forum/index.php?topic=3320.msg19875#msg19875

- [11] The "cbwx34-fix", on Tormekforum Re: Machine Set-up related to carpal tunnel/repetitive motion injuries
- https://bit.ly/2Hy5Vb7
- [12] "Homemade Knife Rest HK-50" by Herman Trivilano ttps://www.tormek.com/forum/index.php?topic=1592
- [13] "Tormek-T7 grinder" folder with several documents https://bit.ly/2KpROFg on OneDrive htt<u>ps://bit.ly/2lHaR3m</u> on DropBox

°. Documentation

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open source office package LibreOffice. It can be downloaded from the public folder "Tormek-T7 grinder" on DropBox and OneDrive. [13] The spreadsheet is titled "USB adjustment table.ods" and is made in the free and

adjustment table.ods" which also can be found in the same folder. holds for the spreadsheet which is used for the tables in Doc1: "Grinding angle Downloaded versions will open and run in Excel. If you upload your own version to the cloud, then it opens and runs also in the online version of Excel. The same

The contents of the folder [13] are:

- Doc1: initial document about mathematical adjustment of the knife jig "Grinding angle adjustment A5 serial.pdf", serial version for tablet "Grinding angle adjustment Booklet.pdf", A5 booklet to be printed on A4
- "Grinding angle adjustment table.ods", spreadsheet for tables in **Doc1**
- "Measuring distance 'S'.JPG", picture of simple measurement of USB-to-stone distance
- This document:
- "More math for the Tormek grinder A5 serial.pdf", serial version for tablet
- "More math for the Tormek grinder booklet.pdf", A5 booklet to print on A4
- "USB adjustment table.ods", spreadsheet to generate the new table

Further developments

In April 2014, after some experimenting on several knifes, I decided to introduce the method on the Tormek-forum. [2]

his ideas and created a variety of improvements and alternatives. ble look-up. He called his design the "Ken-jig"[4] . Several forum-members adopted further simplification so that the adjustment could be done without the need for a ta-September 2014. [3] He became a promoter of this method and even developed a The first reaction about the application of this method came from Ken Schroeder in

tance from the top of the support bar to the base of the grinder rather than the dis In March 2016 the method was adapted by "Wootz" (Vadim) by measuring the dis

easier to reproduce. For that purpose he deing away from the wheel. See Figure 2. signed a "frontal vertical base" for sharpen-

gram to calculate the correct height.[5] He Furthermore he developed a computer proages with construction details. length measuring/setting block including imhe also introduces a simple and accurate jig reviewed and discussed in [6] . In that topic made an applet commercially available. It is polishing machines in his workshop and now applies his method to his grinding and

precision, as stated on his website [7] : His grinding results are of unprecedented

usually near 0.05 micron for high-end under 0.1 micron edge apex width, and knives, sharper than a razor." "... the cutting edge we deliver has at or



He expressed his satisfaction in a message to me in which he clearly described the

benefits

proximation into a scientific precision. "After I scripted your formulas, my sharpening turned from guess and ap-

factory angle or by customer's whim Since then I've never failed to set exact edge angle, will it be keeping the

to T8, and then to paper wheels for honing. move the blade I sharpen from stone to stone of different diameters, from T7 If not for your formulas, I wouldn't be able to keep exact edge angle as I

Only thanks to you I now have every edge apex width under 1 micron, typically 60-90 BESS, within 3-5 minutes.

frontal vertical base as a present. could not wish for better recognition, and moreover he also sent me a copy of his

Meanwhile, five years after introduction, it gets widespread attention as a "method" including instruction movies on youtube. [8]

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the USB is one of the paramestone and the jig's center above ters for the adjustment. The distance 'S' between the

error in grinding angle if this a discussion arose on the forum. in the following note:[10] accuracy of this adjustment of 'S' distance of 85mm is set for the ence point which I emphasized ure 1) refers to the correct refer-Doc1 however (as seen in Fighis appears to be 0.6°, according to For a particular set-up this error "wrong" measurement is done. "Jan" made a calculation on the center of the USB. About the in-Figure 3 gives an example how a calculations.[9] Document



is part of the triangle through the knife in the jig. So it should be measured to but a proposal to simplify the jig-setting. the heart of the jig just above the center of the support. Measuring the dis-Please keep in mind that this subject [i.e. method] is not an academic item, tance to the top of the support however will give a negligible error "The distance is measured NOT to the top NOR the center of the support. It

distance 'S' is measured by me in practice between the stone and the middle of the tings the computed angle was compared with the angle set with the "Anglemaster". USB, as shown in figure 3. To get an impression of the resulting error, for a few set from knife edge to the adjustable stop. That is the correct distance as intended. The The distance K is determined via distance A (Figure 1) by measuring the distance

Measuring set-up

Figure 4 gives an illustration of the measuring set-up. As "knife-jig" a steel ruler was used with a thickness of 1mm. The (dark) steel ruler is resting on the USB and ing backlight passing between ruler and angle setter. stone and the USB, until the angle setter fits on the ruler. That is checked by viewwhite ruler. The steel ruler is then shifted, forward or backwards while touching the touches the stone with its end. The distance of the USB to the stone is set with the

Practice makes perfect?

There was then a range of about 10 mm in which the angle appeared to be correctly set. Therefore measurements have been done for angles of 20° and 30° only, with USB distances to the stone of 65, 80 and 95 mm. turned out to be very difficult to accurately position the steel ruler at the right length. The intention was to measure angles of 10°, 20° and 30°. At the angle of 10° it

The anglemaster must be placed close to the end of the ruler during adjustment.

7. New tables

Since the usage of a table is faster and easier than entering the parameters in an app or formula, I have designed a spreadsheet for generating a table based on formula F9. The table gives the USB-to-stone distance as a function of the jig-length The user can set the following parameters: JG in columns and the desired grinding angle Δ in rows. See figure 11.

System parameters

rarely be changed these parameters are independent of the knifes to be sharpened and must

- Stone diameter AS
- Offset JC between the jig's shaft-centre and USB-centre
- Table parameters

the table these parameters determine the start and increment of the rows and columns of

- minimum value for JG, which is in the first column
- increment between columns of JG
- minimum value for the grinding angle Δ , which is on the first row
- increment hetween 3 ve of v

S

		08 a7 77 27 c7 07 83 73 23 23 7	14 62 64 65 67 69 70 72 74 75 77 79	13 61 62 64 66 67 69 70 72 74 76 77	12 59 61 62 64 66 67 69 71 72 74 76	11 58 59 61 63 64 66 68 69 71 73 74	Grinding angle 10 56 58 60 61 63 64 66 68 69 71 73	△(°) USB-center to stone distance (=S=CS)	Angular offset (°) $\partial_{\mathbf{k}}$ = 5,7 5,6 5,5 5,4 5,4 5,4 5,3 5,2 5,1 5,0 5,0 4,9	USB-center to knife edge (mm) CG= 121 123 125 127 129 131 133 135 137 139 141	Jig-length K to knife edge (mm) JG= 120 122 124 126 128 130 132 134 136 138 140	Adjustment table	∆-increment (between rows)= 1 °	Δ -minimum (first row)= 10 °	JG-increment (between columns)= 2 mm	JG-minimum (left column)= 120 mm	Table parameters (to be preset by user)	USB to stone distance (=S=CS) as function of $\ \Delta$ with jig-length (JG) as parameter	Jig-center to USB-center offset (mm) JC= 12 mm	System parameters (to be measured and preset by user)	Simple adjustment of the grinding angle (△) See report "Ginding angle adjustment" and report "More math for the Tormek grinder"	- IIICLEITIETIT DETWEETI TOWS OF A	140 141 141 141 76 76 76 76	ter	ame 136 137 5,0 5,0 5,0 5,0 5,0 5,0 5,0 5,0 5,0 5,0	1120 1120 1134 1135 1135 1135 1135 1135 1135 1135	AG= AG= AG= AG= AG= AG= AG= AG=	ek grit ===SA= ===SA= 130 131 131 131 131 131 131 131 131 131	Torm 128 128 128 128 128 128	→ F Jig-le 126 127 5,4 61 127 63 66 67	math f 124 125 5,5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	(△) mmmmmmmmmmmmmmmmmmmmmmmmmmmmmm 122 5,6 5,8 5,8 5,8 5,8 5,8 5,8 5,8 5,8	rigle (port ") 2240 122 12 12 12 12 12 12 12 12 12 12 12 12	and real and real dispersion of the second	Simple adjustment of the grindin See report "Grinding angle adjustment" i System parameters (to be measured an Stone diatance (=S=CS) as fi Table parameters (to be preset by JG-minimum (left column)= JG-increment (between columns)= A-minimum (first row)= A-increment (between rows)= Jig-length K to knife edge (mm) USB-center to knife edge (mm) USB-center to knife edge (mm) Grinding angle
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over me variable range. This justifies the final conclusion that, with a simple correction, the tables of <i>doc1</i> are useful for alternative measurements of the stone distance.	count. The "cbwx34-fix" gives an offset of 9.5° with a variation of 0.7° at maximum	chosen at the center of the USB, then an offset angle of 5° should be taken into ac-	The maximum error of 0.2° can clearly be neglected. If the reference point is	where the jig rests on the USB.	not chosen on the centerline of the jig but on the contact point	of Doc1 have to be corrected by 2.5° if the measuring point is	This leads to the conclusion that the grinding angles in the tables			133 mm 2.6° 5.2° 10.2°	as function of JC and JG 6 mm 12 mm 24 mm	JC JC	133 to 150 mm. The following table can then be calculated for the values of $\partial_{\mathbf{k}}$:	the distance A in figure 1. Hence distance JG under these conditions will range from	The distance JG in figure 10 equals distance K in figure 1 which is 6 mm less than	trom 139mm to 156mm.	stop can be varied between 108+31 and 125+31 mm, that is	Thus the distance between the knife edge and the adjustable	extends 31mm from the clamp.	the knife to a depth of 14mm. As a consequence the knife edge	Example: (from <i>Doc1</i>) Consider a pooks knife with a width of 45mm. The iin can prin		as given in Doc1 :	125 mm. The width of the knife adds another variable. So let's consider an example	I he length JG is variable with the adjustable stop of the knite-jig. The length A in tig-		of the USB, the distance JC will equal 12 mm. For the "cbwx34-fix" the distance	USB, then the distance JC will equal to 6 mm. With the reference point at the center	If the reference point 'C' is chosen at the contact point where the jig rests on the	Determining 'offset-angle' ∂ _k	increases the grinding angle with respect to the calculated value.	reference point, a correction must be made for the angle ∂_k (Figure 10), which then	different approach to the use of the tables in <i>doc1</i> . With a different choice of that	Previous considerations concerning the choice of the reference point 'C' lead to a	6 Ilsane of existing tables
The measuring accuracy is abc 1mm results in an angular erro	9	30 8	6	9	20 8	6	Angle (m	Adjuste	Stone	shown in the last column.	which D=S+R. The difference w	where it rests on the USB. With	touching the stone to the point	tance from the end of the rule	the measured and derived va	The shaded columns contai	ter of the USB.	tance from the stone to the cer	ment for the angle-setter of the dis	meters. The angle is the adjust	table contain the adjusted para	The first two columns in th	נמוועבא וע, ט, מווע וע ופופו עט ו וע ווזים 1	ated in the following table. Uis	The results are listed and evalu	Results	the USB center.	results to give the distance t	subtracted from the measure	dius of the USB, i.e., 6 mm, wa	USB edge as reference. The ra	fances were measured with th	provided with a slider as ac	with a caliper and the ruler i	The distance S is determine
ut 1mm. It f of 0.8°. Ne	5 131	0 115	96	5 144	0 126	5 107	n) K (mr	Measur	diameter=2		ingle ∆ can ith respect		~	י ד	- Critic					, 'I'	/									0		- huduuluulu	5 60 55 50	000	
has to be n evertheless	27.8	25.86	27.42	18.72	18.76	19.04	1) ∆ (F1)	ed Calc	40mm → R		to the pres		to	gure 4: The		-	100		0,162							K		C				uluuluuluuluula	45 40 40	35	
oted that a measuring error of , the results are disappointing	2.2	3.36	2.58	-1.28	-1.24	-0.96	∆-Angle	ulated	=120		et angle of the anglemaster is	od popording to formula E1 in	a steel ruler	anglemaster applied			.3			9 8 7 8 2 8			a						150	0. 2	1115 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	r. A	b.		

1mm results in an angular error of 0.8°. Nevertheless, the results are disappointing and the errors are so great that an analysis is needed to arrive at a better understanding of the correct adjustment.

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4. Error analysis

A lot of measurements have been made to find out where the measurement errors could come from. For a long time there was apparently a systematic error. The error turned out to be dependent on the thickness and the sharpening angle. The smaller the angle and the thicker the material the larger the error. I finally discovered that by grinding wood with a thickness of 6 mm. After grinding several pieces with different angles, the cause of the error became clear.



Understanding why thickness matters

The distance K was measured before sharpening, so with a blunt instead of a sharp piece of material. As a consequence the tip of the blade will sink to the stone during sharpening, thereby changing the angle with respect to the stone. This is illustrated in Figure 6.



The error is made by adjusting the length K or JG to the edge of the blunt testing blade. In the figure this length is indicated with K_b. The blade has a thickness of t_b. During the grinding, the tip of the blade sinks over a distance t_b to the stone, causing the grinding angle to change. To compensate this, the setting distance should be increased by an additional value K_e. That value is dependant on the blade thickness t_b and the grinding angle Δ .

The equation
$$tan(\Delta) = \frac{t_b}{K_e}$$
 leads to the formula: $K_e = \frac{t_b}{tan(\Delta)}$.

The following table gives an overview of the values of K_e (on grey background) for some combinations of blade thickness and grinding angle. It is clear that this can cause a major error, for example 17 mm at a grinding angle of 10° and blade thickness of 3 mm.

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Resulting grinding angle Δ

An expression for the grinding angle Δ can directly be derived from formula F9. The first step is squaring, to eliminate the square root, and then rearrange the terms:

$$2*CG*AG*sin(\Delta-arctan(JC/JG))=CA^2-CG^2-AG^2$$

Separation of the trigonometric function gives:

$$sin(\Delta-arctan(JC/JG)) {=} \frac{CA^2 {-} CG^2 {-} AG^2}{2*CG*AG}$$

That leads to the inverse trigonometric function:

$$\arctan(JC/JG) = \Delta - \arcsin\left(\frac{CA^2 - CG^2 - AG^2}{2*CG*AG}\right)$$
 [F12]

and rearranging the terms results in the function for Δ :



Usage with other reference points

The reference point 'C' in figure 10 is chosen as being the center of the USB. However, the formulas remain the same if the reference point is chosen elsewhere, for example on the top of the USB or the point where the knife-jig rests on the USB, the "contact point". Of course, different distances will then change, but as long as the rectangular angles remain intact, the formulas remain valid.

If the reference point '**C**' is chosen at the center of the knife-jig as in figure 1, then the distance JC reduces to zero and formula F14 reduces then to formula F1. As a consequence the tables in **Doc1**, which are related to formula F1, can also be

As a consequence the tables in **Loc 7**, which are related to formula F1, can also be applied with an offset JC if a correction is made for the 'offset-angle' ∂_k in figure 10 which equals the term arctan(JC/JG) in formula F14.

It will be clea two-sided gri sharpened bla Error by inc Figure 7 is a ing set-up of rulers rest on which measu	It will be clean two-sided gri sharpened bla Error by inc Figure 7 is a ing set-up of rulers rest on which measu	It will be clean two-sided gri sharpened bla Error by inc Figure 7 is a ing set-up of rulers rest on which measu	It will be clea two-sided gri sharpened bla Figure 7 is a ing set-up of rulers rest on which measu	It will be clea two-sided gri sharpened bla Error by inc Figure 7 is a ing set-up of rulers rest on which measu	It will be clea two-sided gri sharpened bla Figure 7 is a ing set-up of rulers rest on which measu	It will be clea two-sided gri sharpened bla Error by inc Figure 7 is a ing set-up of rulers rest on which measu
ar that only half the blade thickness has to be taken into account for prinding. Furthermore this error is not present or negligible with lades. Icorrect reference point a schematic representation of the measur-	blade thickness t_b and angle Δ ar that only half the blade thickness has to be taken into account for prinding. Furthermore this error is not present or negligible with lades. Icorrect reference point a schematic representation of the measur- of Figure A It shows where the K and S	Extension K _e of jig-length as function of blade thickness t _b and angle ∆ ar that only half the blade thickness has to be taken into account for prinding. Furthermore this error is not present or negligible with lades. Icorrect reference point a schematic representation of the measur-	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\frac{\Delta (^{\circ})}{10} 1 2 3 4 5 6 \\ \hline 10 5.7 11.3 17.0 22.7 28.4 34.0 \\ \hline 15 3.7 7.5 11.2 14.9 18.7 22.4 \\ \hline 20 2.7 5.5 8.2 11.0 13.7 16.5 \\ \hline 25 2.1 4.3 6.4 8.6 10.7 12.9 \\ \hline 30 1.7 3.5 5.2 6.9 8.7 10.4 \\ \hline Extension K_{e} \text{ of jig-length as function of blade thickness } t_{b} \text{ and angle } \Delta \\ \hline Extension K_{e} \text{ of jig-length as to be taken into account for blade thickness has to be taken into account for negligible with lades. \\ \hline \text{Icorrect reference point} \\ a \text{ schematic representation of the measur-} \\ \hline K \\ \hline \text{Figure A It is how we where the K and S} \\ \hline \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$
It will be clear that only half the blade thickness has to be taken into account for two-sided grinding. Furthermore this error is not present or negligible with sharpened blades	It will be clear that only half the blade thickness t_b and angle Δ two-sided grinding. Furthermore this error is not present or negligible with	Extension K_e of jig-length as function of blade thickness t_b and angle Δ It will be clear that only half the blade thickness has to be taken into account for two-sided grinding. Furthermore this error is not present or negligible with	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	It will be clear that only half the blade thickness has to be taken into account for two-sided grinding. Furthermore this error is not present or negligible with	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$ \frac{\Delta (^{\circ})}{10} 1 2 3 4 5 6 \\ \hline 10 5.7 11.3 17.0 22.7 28.4 34.0 \\ \hline 15 3.7 7.5 11.2 14.9 18.7 22.4 \\ \hline 20 2.7 5.5 8.2 11.0 13.7 16.5 \\ \hline 25 2.1 4.3 6.4 8.6 10.7 12.9 \\ \hline 30 1.7 3.5 5.2 6.9 8.7 10.4 \\ \hline \text{Extension } K_e \text{ of } jig-length as function of \\ blade thickness t_b and angle \Delta \\ \hline \text{It will be clear that only half the blade thickness has to be taken into account for two-sided grinding. Furthermore this error is not present or negligible with separate blades \\ \hline \end{tabular} $
	blade thickness $\mathbf{t}_{\mathbf{b}}$ and angle Δ	Extension K_e of jig-length as function of blade thickness t_b and angle Δ	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

spect to the original line segment K and is the offset with respect to the grinding angle determined by ${\sf K}_r$ and ${\sf S}_r.$ ingular offset with re-

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So in principle the grinding angle could be determined by applying the cosine rule with distances K_r and S_r , but then the angle to be set must be reduced by the offset ∂_k . In addition, there is also an extra offset because the centerline of the jig is 6 mm above the USB.

Another reason to pay more attention to the "offset" between the jig and the USB was the development of a robust attachment of the knife-jig to the USB by forum member "cbwx34". [11] . I call it after the developer's forum-name "*cbwx34-fix*". It is displayed in Figure 9.



. Grinding angle adjustment for the "cbwx34-fix"

In his method with "the frontal vertical base" (Figure 2) "Wootz" sets the USB-height with respect to the grinder-base. According to his information, the applet for the adjustment takes the offset into account. As the math behind this correction was not published on the forum, "cbwx34" (Curtis) contacted me for help on the adjustment of the jig in his "cbwx34-fix".

The adjustment formula will be derived with reference to the following figure which is a schematic representation of the "*cbwx34-fix*" as displayed in Figure 9.



The numbering of the formulas is a continuation of the numbering in **Doc1**. The angle Δ is the grinding angle and equals Angle ∂_k is adjustable via the length JG with the adjustable stop of the knife-jig. Angle α_2 equals $\alpha_2 = \alpha_1 - 90^\circ$ in which α_1 is adjustable via the length BC with the